## Traffic Terms"and Concepts

Why do we need to concern ourselves with traffic when we design pavements? Traffic is what LOADS the pavement


- Repeated, cyclic loads on a structure eventually result in structural fatigue



# We see the result of this fatigue as pavement damage or distress. 

Concept of load equilivalency ansl standard unit load/configuracion used in pavement design technology.

- Heavy vehicles cause damage to pavements
- The heavier the load per axle, the more damage
- In order to assess the damage caused by the many different types/configurations of vehicles, one specific load/configuration has been adopted as the standard

- The standard adopted is the $18,000 \mathrm{lb}$ single axle load, a truck with a single rear axle
- The rear wheels each transmit 9000 bloads to


9000 lb
$18,000 \mathrm{lb}=80 \mathrm{kN}$

- A load equivalency factor gives thene nusniber of repetitions of the standard load/configuraition that would cause an equivalent amount of clamage as one pass of the specific venicle;
e.g., a load equivalency factor of 2.5 rneans thaic...

one pass of a specific vehicle

causes an equivalent amount of damage as two and a half passes of the standard vehicle
a) ESAL
b) ITN
c) DTN
a) the standard load and axle configuration to which all other load and axle configurations are converted when evaluating traffic loads for pavement structural design

ESAL = Equivalent Single Axle Load


## ITN (Initial Traffic Number)

- the average number of ESAL's/day in the first year of a pavement design analysis period


## DTN (Design Traffic Number) <br> \section*{}

- the average number of ESALL's/day over the entire pavement design analysis period
- The total ESAL applications over the design analysis period divided by the number of traffic
days
egg, 6,000,000 ESAL's over 20 years $=300,000$
ESAL's per year or 1,000 ESAL's per day for 300
e.g, $6,000,000$ ESAL's over 20 years $=300,000$
ESAL's per year or 1,000 ESAL's per day for 300 truck days per year ( $(\mathrm{i}, \mathrm{e}, \mathrm{DTN}=1000$ ) slay over the
 $+\frac{2}{2}+e^{2}$



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## Load distribution through the pavement structure



Typical assumptions:

- Multilayered elastic system
- Subbase, base course, AC surface is infinite in the horizontal direction
- Subgrade is infinite in the vertical and horizontal direction
- Contain both the horizontal and vertical strains below the set values that will cause excessive cracking
- These criteria are considered in terms of repeated load applications because the accumulated repetitions of traffic loads are of significant importance to the development of cracks and permanent deformation of the
 pavement.


## Estimating accumulated wheel load repetitions

Traffic Characteristics: The traffic characteristics are determined in terms of the number of repetitions of an 18,000-lb (80 kilo-newtons ( kN ) ) single-axle load applied to the pavement on two sets of dual tires.


Equivalent single-axle load (ESAL)

- Tire contact area (each 4.51 in . ( 11 cm ) radius) and $13.57(33 \mathrm{~cm})$ in apart

Contact pressure of 70 $\mathrm{lb} / \mathrm{in}^{2}$


Premise: "the effect of any load on the performance of a pavement can be represented in terms of the number of single applications of an 18,000-lb single axle.

4 tires x $\pi \times 4.51^{2}=255.601 \mathrm{in}^{2}$, Total single-axle load $=255.601 \times 70$ $\mathrm{lb} / \mathrm{in}^{2}=17,892$ approximately $18,000 \mathrm{lbs}$.

## Load equivalency factors (Table 20.3): Use this if you know axle loads

Gross Axle Load
Load Equivalency Factors
Single Axles Tandem Axles Tridem Axles

| 4.45 | 1,000 | 0.00002 |  |  |
| ---: | ---: | :--- | :--- | :--- |
| 8.9 | 2,000 | 0.00018 |  |  |
| 17.8 | 4,000 | 0.00209 | 0.0003 | 0.0003 |
| 26.7 | 6,000 | 0.01043 | 0.001 | 0.001 |
| 35.6 | 8,000 | 0.0343 | 0.003 | 0.002 |
| 44.5 | 10,000 | 0.0877 | 0.007 | 0.003 |
| 53.4 | 12,000 | 0.189 | 0.014 | 0.006 |
| 62.3 | 14,000 | 0.360 | 0.027 | 0.011 |
| 71.2 | 16,000 | 0.623 | 0.047 | 0.017 |
| 8.0 | 18,000 | 1.000 | 0.077 | 0.027 |
| 89.0 | 20,000 | 1.51 | 0.121 |  |

Obviously the traffic mix (cars, buses, SU trucks, semis, etc.) must be known because their gross axle loads are different. $\rightarrow$ Vehicle classification counts are needed. Also needed is axle load data - the reason for having truck weighing stations on major highways.

## How to estimate the traffic mix if field data are not available (In this case axle loads data must be available).

Table 20.4 can help you estimate break-down of truck types in percentages.

## Rural Systems

| Truck Class |  | Other | Minor |  | tors |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Interstate | Principal | Arterial | Major | Minor | Range |
| Single-unit trucks |  |  |  |  |  |  |
| 2-axle, 4-tire | 43 \% | 60 | 71 | 73 | 80 | 43-80 |
| 2-axle, 6-tire | 8 | 10 | 11 | 10 | 10 | 8-11 |
| 3-axle or more | 2 | 3 | 4 | 4 | 2 | $2-4$ |
| All single-units | 53 | 73 | 86 | 87 | 92 | 53-92 |
| Multiple-unit trucks |  |  |  |  |  |  |
| 4-axle or less | 5 | 3 | 3 | 2 | 2 | 2-5 |
| 5-axle** | 41 | 23 | 11 | 10 | 6 | 6-41 |
| $\begin{aligned} & \text { 6-axle or } \\ & \text { more }{ }^{\star \star} \end{aligned}$ | 1 | 1 | $<1$ | 1 | $<1$ | $<1-1$ |
| All multiple units | 47 | 27 | 14 | 13 | 8 | 8-47 |
| All trucks | $100 \%$ | 100 | 100 | 100 | 100 |  |

## How to estimate ESAL if axle loads are not known

The equivalent $18,000-\mathrm{lb}$ loads can also be determined from the vehicle type, if the axle load is unknown, by using a truck factor for that vehicle type. The truck factor is defined as the number of $18,000-\mathrm{lb}$ single-load applications caused by a single passage of a vehicle.

Table 20.5 gives truck factors, that is, they were computed based on previous research data. Remember this formula as the definition of the truck factor. You may not actually compute it unless you are determining typical truck factors for your study area. Problem 20-4 let you use this formula.


## Distribution of truck factors for different classes of highways and vehicles

Rural Systems

| Vehicle | Other | Minor | Collectors |  |
| :---: | :---: | :---: | :---: | :---: |
| Type | Interstate Principal | Arterial | Major | Minor | Range


| Single-unit trucks |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2-axle, 4-tire | 0.003 | 0.003 | 0.003 | 0.017 | 0.003 | 0.003-0.017 |
| 2-axle, 6-tire | 0.21 | 0.25 | 0.28 | 0.41 | 0.19 | 0.19-0.41 |
| 3-axle or more | 0.61 | 0.86 | 1.06 | 1.26 | 0.45 | 0.45-1.26 |
| All single-units | 0.06 | 0.08 | 0.08 | 0.12 | 0.03 | 0.03-0.12 |
| Tractor-semitrailers |  |  |  |  |  |  |
| 4 -axle or less | 0.62 | 0.92 | 0.62 | 0.37 | 0.91 | 0.37-0.91 |
| 5-axle ${ }^{\text {® }}$ | 1.09 | 1.25 | 1.05 | 1.67 | 1.11 | 1.05-1.67 |
| 6 -axle or more ${ }^{\star \star}$ | 1.23 | 1.54 | 1.04 | 2.21 | 1.35 | 1.04-2.21 |
| All multiple units | 1.04 | 1.21 | 0.97 | 1.52 | 1.08 | 0.97-1.52 |
| All trucks | 0.52 | 0.38 | 0.21 | 0.30 | 0.12 | 0.12-0.52 |

Example: For rural interstates, one single truck is considered to have 0.52 ESAL. Count the total number of trucks and multiply it by 0.52 to find total ESAL for that section.

## Determining the accumulated ESAL

Must know: Design period, traffic growth rate, and design lane factor. Usually a 20 -year design period is used. Traffic growth rates can be obtained from the planning division of the State DOT.

## Table 20.6 <br> Growth Factors



## Determining accumulated ESAL when axle loads are used

## $E S A L_{i}=f_{d} \times G_{j t} \times A A D T_{i} \times 365 \times N_{i} \times F_{E i}$

* $\mathrm{ESAL}_{\mathrm{i}}=$ equivalent accumulated $18,000-\mathrm{lb}(80 \mathrm{kN})$ single-axle load for the axle category i
* $\mathrm{f}_{\mathrm{d}}=$ design lane factor
* $\mathrm{G}_{\mathrm{jt}}=$ growth factor for a given growth rate j and design period t
* $\mathrm{AADT}_{\mathrm{i}}=$ first year annual average daily traffic for axle category i
* $\mathrm{N}_{\mathrm{i}}=$ number of axles on each vehicle in axle category i
* $\mathrm{F}_{\mathrm{Ei}}=$ load equivalency factor for axle category i

Note that AADT used here is the total for both directions.

## Determining accumulated ESAL when truck factors are used

$$
E S A L_{i}=f_{d} \times G_{j t} \times A A D T_{i} \times 365 \times f_{i}
$$

The accumulated ESAL for all categories of axle loads is:

$$
E S A L=\sum_{i=1}^{n}\left[E S A L_{i}\right]
$$

* $\mathrm{ESAL}_{\mathrm{i}}=$ equivalent accumulated $18,000-\mathrm{lb}$ axle load for truck category i
* $\mathrm{f}_{\mathrm{d}}=$ design lane factor
* $\mathrm{G}_{\mathrm{jt}}=$ growth factor for a given growth rate j and design period t
* $\mathrm{AADT}_{\mathrm{i}}=$ first year annual average daily traffic for truck category i
* $\mathrm{f}_{\mathrm{i}}=$ truck factor for vehicles in truck category i
* ESAL = equivalent accumulated $18,000-\mathrm{lb}$ axle loads for all vehicles
* $\mathrm{n}=$ number of truck categories

| $\text { Table } 20.3$ |  | Equivalent axle load factor |  |  | Axle load <br> (lb) | Equivalent axle load factor |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | load <br> (lb) | Single axles | Tandem axles | Tridem axles |  | Single axles | Tandem axles | Tridem axles |
|  | 1000 | 0.00002 |  |  | 41,000 | 23.27 | 2.29 | 0.540 |
|  | 2000 | 0.00018 |  |  | 42,000 | 25.64 | 2.51 | 0.597 |
|  | 3000 | 0.00072 |  |  | 43,000 | 28.22 | 2.76 | 0.658 |
|  | 4000 | 0.00209 |  |  | 44,000 | 31.00 | 3.00 | 0.723 |
|  | 5000 | 0.00500 |  |  | 45,000 | 34.00 | 3.27 | 0.793 |
|  | 6000 | 0.01043 |  |  | 46,000 | 37.24 | 3.55 | 0.868 |
|  | 7000 | 0.0196 |  |  | 47,000 | 40.74 | 3.85 | 0.948 |
|  | 8000 | 0.0343 |  |  | 48,000 | 44.50 | 4.17 | 1.033 |
|  | 9000 | 0.0562 |  |  | 49,000 | 48.54 | 4.51 | 1.12 |
|  | 10,000 | 0.0877 | 0.00688 | 0.002 | 50,000 | 52.88 | 4.86 | 1.22 |
|  | 11,000 | 0.1311 | 0.01008 | 0.002 | 51,000 |  | 5.23 | 1.32 |
|  | 12,000 | 0.189 | 0.0144 | 0.003 | 52,000 |  | 5.63 | 1.43 |
|  | 13,000 | 0.264 | 0.0199 | 0.005 | 53,000 |  | 6.04 | 1.54 |
|  | 14,000 | 0.360 | 0.0270 | 0.006 | 54,000 |  | 6.47 | 1.66 |
|  | 15,000 | 0.478 | 0.0360 | 0.008 | 55,000 |  | 6.93 | 1.78 |
|  | $16,000$ | 0.623 | 0.0472 | 0.011 | 56,000 |  | 7.41 | 1.91 |
|  | $17,000$ | 0.796 | 0.0608 | 0.014 | 57,000 |  | 7.92 | 2.05 |
|  | 18,000 | 1.000 | 0.0773 | 0.017 | 58,000 |  | 8.45 | 2.20 |
|  | 19,000 | 1.24 | 0.0971 | 0.022 | 59,000 |  | 9.01 | 2.35 |
|  | 20,000 | 1.51 | 0.1206 | 0.027 | 60,000 |  | 9.59 | 2.51 |
|  | 21,000 | 1.83 | 0.148 | 0.033 | 61,000 |  | 10.20 | 2.67 |
|  | 22,000 | 2.18 | 0.180 | 0.040 | 62,000 |  | 10.84 | 2.85 |
|  | 23,000 | 2.58 | 0.217 | 0.048 | 63,000 |  | 11.52 | 3.03 |
|  | 24,000 | 3.03 | 0.260 | 0.057 | 64,000 |  | 12.22 | 3.22 |
|  | 25,000 | 3.53 | 0.308 | 0.067 | 65,000 |  | 12.96 | 3.41 |
|  | $26,000$ | 4.09 | 0.364 | 0.080 | 66,000 |  | 13.73 | 3.62 |
|  | $27,000$ | 4.71 | 0.426 | 0.093 | 67,000 |  | 14.54 | 3.83 |
|  | 28,000 | 5.39 | 0.495 | 0.109 | 68,000 |  | 15.38 | 4.05 |
|  | 29,000 | 6.14 | 0.572 | 0.126 | 69,000 |  | 16.26 | 4.28 |
|  | 30,000 | 6.97 | 0.658 | 0.145 | 70,000 |  | 17.19 | 4.52 |
|  | 31,000 | 7.88 | 0.753 | 0.167 | 71,000 |  | 18.15 | 4.77 |
|  | 32,000 | 8.88 | 0.857 | 0.191 | 72,000 |  | 19.16 | 5.03 |
|  | 33,000 | 9.98 | 0.971 | 0.217 | 73,000 |  | 20.22 | 5.29 |
|  | 34,000 | 11.18 | 1.095 | 0.246 | 74,000 |  | 21.32 | 5.57 |
|  | 35,000 | 12.50 | 1.23 | 0.278 | 75,000 |  | 22.47 | 5.86 |
|  | $36,000$ | 13.93 | 1.38 | 0.313 | 76,000 |  | 23.66 | 6.15 |
|  | 37,000 | 15.50 | 1.53 | 0.352 | 77,000 |  | 24.91 | 6.46 |
|  | 38,000 | 17.20 | 1.70 | 0.393 | 78,000 |  | 26.22 | 6.78 |
|  | 39,000 | 19.06 | 1.89 | 0.438 | 79,000 |  | 27.58 | 7.11 |
|  | 40,000 | 21.08 | 2.08 | 0.487 | 80,000 |  | 28.99 | 7.45 |

Note. $1 \mathrm{lb}=4.45 \mathrm{~N}$.

| Table 20.6 | Design period (years) | Annual growth rate (\%) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | No growth | 2 | 4 | 5 | 6 | 7 | 8 | 10 |
|  | 1 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
|  | 2 | 2.0 | 2.02 | 2.04 | 2.05 | 2.06 | 2.07 | 2.08 | 2.10 |
|  | 3 | 3.0 | 3.06 | 3.12 | 3.15 | 3.18 | 3.21 | 3.25 | 3.31 |
|  | 4 | 4.0 | 4.12 | 4.25 | 4.31 | 4.37 | 4.44 | 4.51 | 4.64 |
|  | 5 | 5.0 | 5.20 | 5.42 | 5.53 | 5.64 | 5.75 | 5.87 | 6.11 |
|  | 6 | 6.0 | 6.31 | 6.63 | 6.80 | 6.98 | 7.15 | 7.34 | 7.72 |
|  | 7 | 7.0 | 7.43 | 7.90 | 8.14 | 8.39 | 8.65 | 8.92 | 9.49 |
|  | 8 | 8.0 | 8.58 | 9.21 | 9.55 | 9.90 | 10.26 | 10.64 | 11.44 |
|  | 9 | 9.0 | 9.75 | 10.58 | 11.03 | 11.49 | 11.98 | 12.49 | 13.58 |
|  | 10 | 10.0 | 10.95 | 12.01 | 12.58 | 13.18 | 13.82 | 14.49 | 15.94 |
|  | 11 | 11.0 | 12.17 | 13.49 | 14.21 | 14.97 | 15.78 | 16.65 | 18.53 |
|  | 12 | 12.0 | 13.41 | 15.03 | 15.92 | 16.87 | 17.89 | 18.98 | 21.38 |
|  | 13 | 13.0 | 14.68 | 16.63 | 17.71 | 18.88 | 20.14 | 21.50 | 24.52 |
|  | 14 | 14.0 | 15.97 | 18.29 | 19.16 | 21.01 | 22.55 | 24.21 | 27.97 |
|  | 15 | 15.0 | 17.29 | 20.02 | 21.58 | 23.28 | 25.13 | 27.15 | 31.77 |
|  | 16 | 16.0 | 18.64 | 21.82 | 23.66 | 25.67 | 27.89 | 30.32 | 35.95 |
|  | 17 | 17.0 | 20.01 | 23.70 | 25.84 | 28.21 | 30.84 | 33.75 | 40.55 |
|  | 18 | 18.0 | 21.41 | 25.65 | 28.13 | 30.91 | 34.00 | 37.45 | 45.60 |
|  | 19 | 19.0 | 22.84 | 27.67 | 30.54 | 33.76 | 37.38 | 41.45 | 51.16 |
|  | 20 | 20.0 | 24.30 | 29.78 | 33.06 | 36.79 | 41.00 | 45.76 | 57.28 |
|  | 25 | 25.0 | 32.03 | 41.65 | 47.73 | 54.86 | 63.25 | 73.11 | 98.35 |
|  | 30 | 30.0 | 40.57 | 56.08 | 66.44 | 79.06 | 94.46 | 113.28 | 164.49 |
|  | 35 | 35.0 | 49.99 | 73.65 | 90.32 | 111.43 | 138.24 | 172.32 | 271.02 |


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